# RADIO ENGINEERING <br> MICROWAVE RADIO <br> INTERFERENCE <br> <br> 2-GHZ SYSTEMS 

 <br> <br> 2-GHZ SYSTEMS}
to-interference tables and the application of baseband interference spectrum plots in determination of C/I values. Reference to this section can be made regarding interpretation of data herein contained.
2. RECOMMENDED FREQUENCY AND CHANNEL-
IZATION PLAN

## A. Frequency and Channelization

2.01 The $2-\mathrm{GHz}$ frequency bands of interest (2110 to 2130 MHz and 2160 to 2180 MHz ) do not have specific channel assignments as specified by the FCC, and are therefore open to optional channel assignments. In order to provide uniformity in the selection and application of $2-\mathrm{GHz}$ channel frequencies throughout the Bell System, the following frequency and channelization plan has been established. The purpose of this plan (as shown below) is to obtain the highest capacity consistent with flexibility and high quality performance. As such, the plan uses the maximum authorized channel bandwidth of 3.5 MHz , permitting five channels each in the respective low and high bands with a $3.6-\mathrm{MHz}$ center-to-center channel spacing.

| CHAN NO. | FREQ (LOW) | CHAN NO. | FREQ (HIGH) |
| :---: | :---: | :---: | :---: |
| 1 A | 2113.8 | 1 B | 2163.8 |
| 2 A | 2117.4 | 2 B | 2167.4 |
| 3 A | 2121.0 | 3 B | 2171.0 |
| 4 A | 2124.6 | 4 B | 2174.6 |
| 5A | 2128.2 | 5 B | 2178.2 |

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Bell System except under written agreement

## B. Implementation

2.02 The recommended diplexing arrangement is shown in Fig. 1. This arrangement allows the upper frequency to be transmitted (or received) on either of the two polarizations while the lower frequency band is received (or transmitted) on the opposite polarization. With this suggested utilization, three 2 -way channels are available using a single antenna. It is then possible to add two additional channels to the route by equipping a second antenna.

## 3. INTERFERENCE OBJECTIVES

## A. Rationale and Methodology

3.01 The C/I objectives as contained in Tables C through $G$ were generated for use in the microwave interference computer program (MICPGM). The calculation considers the frequency tolerances of the wanted and unwanted systems to compute the maximum frequency drift of both systems combined. Computations are then made in $1.2-\mathrm{MHz}$ increments, resulting in the $\mathrm{C} / \mathrm{I}$ objectives selected for the frequency separations specified in Table A, and which comprise the separations of Tables C through G. The computer program is designed so as to yield the worst case objective for a given combination of radio systems.
3.02 While the selected frequency separations are designed to be compatible with the recommended Bell System frequency plan (note, for example, the adjacent channel separation at 3.6 MHz ), the absence of specific FCC channel assignments permits almost any separations between 0 and 20 MHz as possibilities. Interferences at intermediate values say, for example, occurring at 2.8 MHz in the $2.4-$ to 3.6 MHz range, take the objective specified in the $2.4-$ MHz table. Although some error will result, the error will be conservative. The closer the difference comes to equaling the computed separation, the more accurate the designated objective. (There is one exception to this, as will be subsequently discussed in conjunction with carrier beat interference and the $0-\mathrm{MHz}$ separation objectives.)
3.03 The objectives were computed on the basis of the short-haul noise allocation of 14 dBrnc 0 per exposure, and an average talker power level of -19.6 dBm was assumed. Carrier beat interference (see Section 940-330-105 for an explanation of carrier beat phenomena) has been taken into account in computation of the objectives and, therefore, is not itemized as distinct from continuous or sideband objectives. The only exception to this is the cochannel or $0-\mathrm{MHz}$ separation case for FM systems only. FM channels that are exactly cochannel take a smaller objective number than other separations between 0 and 1.2 MHz . This special case is handled by providing the "exactly 0 separation objective" along with the worst case objective on the attached matrix for $0-\mathrm{MHz}$ separation. Two conditions must be met to use this objective. First, the wanted and unwanted systems must operate at exactly the same frequency, and second, the combined frequency drift must be no greater than the bottom baseband frequency of the wanted system. (Normally, carrier beat objectives are larger than continuous objectives. However, if the drift does not exceed the bottom baseband frequency, the condition will approximate zero beat.)

## B. 2-GHz FM Radio System Characteristics

3.04 The characteristics of $2-\mathrm{GHz}$ FM systems appear in Table B. The remaining systems are digital.

## C. C/I Objectives

3.05 The C/I objectives are presented in Tables C, D, E, F, and G as follows:

Table C $-0.0-\mathrm{MHz}$ separation
Table D $-1.2-\mathrm{MHz}$ separation
Table $\mathrm{E}-2.4-\mathrm{MHz}$ separation
Table $\mathrm{F}-3.6-\mathrm{MHz}$ separation
Table G $-4.8-\mathrm{MHz}$ separation.


Fig. 1-2-GHz Channelization Implementation

TABLE A

SELECTED C/I OBJECTIVES

| result of computation | C/I objective selected |
| ---: | :---: |
| 0 MHz to 1.2 MHz | $0-\mathrm{MHz}$ Matrix |
| 1.2 MHz to 2.4 MHz | 1.2-MHz Matrix |
| 2.4 MHz to 3.6 MHz | $2.4-\mathrm{MHz}$ Matrix |
| 3.6 MHz to 4.8 MHz | $3.6-\mathrm{MHz}$ Matrix |
| 4.8 MHz to 6.0 MHz | $4.8-\mathrm{MHz}$ Matrix |
| 6.0 MHz to 20 MHz | Default to 20 dB |

TABLE B
2-GHz FM RADIO SYSTEM CHARACTERISTICS

| SYSTEM | CHANNEL <br> CAPACITY | TOP <br> BASEBAND <br> FREQUENCY <br> $(\mathbf{M H z})$ | BOTTOM <br> BASEBAND <br> FREQUENCY <br> $(\mathbf{M H z})$ | TOTAL RMS <br> FREQUENCY <br> DEVIATION <br> $(\mathbf{k H z})$ | PRE-EMPHASIS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| FM-72 | 72 | .300 | .023 | 238 | CCIR |
| FM-132 | 132 | .552 | .012 | 188 | CCIR |
| FM-252 | 252 | 1.052 | .012 | 116 | CCIR |

table C

## 2-GHz INTERFERENCE OBJECTIVES O.O-MHz SEPARATION

INTERFERED-WITH SYSTEMS

|  | SYSTEM | 72 | 132 | 252 | NEC-STD | NEC-HI | DR2C | DR2D | FARINON DMI/2 | VIDAR DRM2-6 | Lenkurt 79F1-D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INTERFERING SYSTEMS | 72 | 46/45 | 55(54) | 69(63) | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | 132 | 45 | 59(52) | 74(61) | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | 252 | 46 | 62(54) | 75(62) | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | NEC-STD | 46/42 | 52 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | NEC-HI | 46/42 | 52 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | DR2C | 46/42 | 52 | 64 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | DR2D | 46/40 | 51 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | FARINON DMI/2 | 46/42 | 52 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | VIDAR DRM2-6 | 46/43 | 53 | 64 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
|  | LENKURT 79FI-D | 46/43 | 53 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |

Note 1: $\mathrm{AA}(\mathrm{BB}) \quad \mathrm{BB}$-Exactly $0.0-\mathrm{MHz}$ separation and high stability AA-Anywhere else

Note 2: $\mathrm{XX} / \mathrm{YY}-\mathrm{XX}$ is a threshold degradation number based on a $40-\mathrm{dB}$ typical fade margin for nominal system IF filtering in the analog group. The objective may be relaxed dB for dB up to YY for lesser fade margins.

TABLE D

## 2-GHz INTERFERENCE OBJECTIVES

## 1.2-MHz SEPARATION

INTERFERED-WITH SYSTEMS

|  | SYSTEM | 72 | 132 | 252 | NEC-STD | NEC-HI | DR2C | DR2D | FARINON DMI/2 | VIDAR DRM2-6 | LENKURT 79F1-D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 72 | 46/30 | 46/45 | 67 | 64 | 64 | 59 | 62 | 65 | 65 | 64 |
|  | 132 | 45/30 | 45/43 | 65 | 64 | 63 | 58 | 61 | 48 | 64 | 64 |
|  | 252 | 45/27 | 45/41 | 59 | 64 | 63 | 58 | 62 | 44 | 64 | 65 |
|  | NEC-STD | 46/38 | 49 | 62 | 64 | 63 | 60 | 62 | 59 | 64 | 63 |
|  | NEC-HI | 46/38 | 49 | 62 | 64 | 63 | 60 | 62 | 59 | 64 | 63 |
|  | DR2C | 46/38 | 49 | 62 | 64 | 63 | 60 | 62 | 59 | 64 | 63 |
|  | DR2D | 46/38 | 49 | 63 | 65 | 64 | 61 | 63 | 59 | 64 | 63 |
|  | FARINON DMI/2 | 46/40 | 50 | 61 | 64 | 63 | 61 | 62 | 61 | 63 | 62 |
|  | VIDAR DRM2-6 | 46/38 | 49 | 62 | 64 | 63 | 60 | 63 | 59 | 64 | 63 |
|  | LENKURT 79FI-D | 46/37 | 48 | 64 | 65 | 63 | 60 | 62 | 58 | 62 | 63 |

Note: $\mathrm{XX} / \mathrm{YY}-\mathrm{XX}$ is a threshold degradation number based on a 40-dB typical fade margin for nominal system IF filtering in the analog group. The objective may be relaxed $d B$ for $d B$ up to YY for lesser fade margins.

TABLE E
2-GHZ INTERFERENCE OBJECTIVES
2.4-MHz SEPARATION

INTERFERED-WITH SYSTEMS

|  | SYSTEM | 72 | 132 | 252 | NEC-STD | NEC-HI | DR2C | DR2D | FARINON DMI/2 | $\begin{aligned} & \text { VIDAR } \\ & \text { DRM2-6 } \end{aligned}$ | LENKURT <br> 79FI-D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 72 | 45/20 | 45/20 | 45/40 | 60 | 52 | 27 | 46 | 20 | 60 | 38 |
|  | 132 | 44/20 | 44/20 | 44/37 | 59 | 50 | 27 | 45 | $\underline{20}$ | 60 | 37 |
|  | 252 | 44/20 | 44/20 | 44/31 | 59 | 49 | 29 | 43 | $\underline{20}$ | 61 | 40 |
|  | NEC-STD | 45/20 | 45/30 | 54 | 61 | 57 | 48 | 55 | 34 | 51 | 56 |
|  | NEC-HI | 45/20 | 45/30 | 54 | 61 | 57 | 48 | 55 | 34 | 51 | 56 |
|  | DR2C | 45/20 | 45/30 | 54 | 61 | 57 | 48 | 55 | 27 | 51 | 55 |
|  | DR2D | 45/20 | 45/29 | 53 | 62 | 57 | 47 | 54 | 28 | 52 | 55 |
|  | FARINON DMI/2 | 45/24 | 45/38 | 60 | 61 | 59 | 53 | 57 | 43 | 46 | 58 |
|  | VIDAR DRM2-6 | 45/20 | 45/31 | 53 | 61 | 57 | 48 | 55 | 28 | 52 | 55 |
|  | LENKURT 79FI-D | 45/20 | 45/31 | 51 | 61 | 56 | 46 | 53 | 38 | 51 | 53 |

Note 1: All underlined objectives are floor numbers.
Note 2: $\mathrm{XX} / \mathrm{YY}-\mathrm{XX}$ is a threshold degradation number based on a $40-\mathrm{dB}$ typical fade margin for nominal system IF filtering in the analog group. The objective may be relaxed dB for dB up to YY for lesser fade margins.

TABLE F

## 2-GHz INTERFERENCE OBJECTIVES

$3.6-\mathrm{MHz}$ SEPARATION
INTERFERED-WITH SYSTEMS

|  | SYSTEM | 72 | 132 | 252 | NEC-STD | NEC-HI | DR2C | DR2D | FARINON DMI/2 | VIDAR DRM2-6 <br> DRM2-6 | LENKURT <br> 79F1-D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 72 | 41/20 | 41/20 | 41/20 | 42 | 20 | 20 | 20 | 21 | 41 | 25 |
|  | 132 | 41/20 | 41/20 | 41/20 | 40 | $\underline{20}$ | 20 | 20 | 21 | 42 | 25 |
|  | 252 | 41/20 | 41/20 | 41/20 | 38 | $\underline{20}$ | 20 | 20 | 20 | 43 | 26 |
|  | NEC-STD | 41/20 | 41/20 | 41/30 | 52 | 44 | $\underline{20}$ | 32 | 21 | 31 | 28 |
|  | NEC-H | 41/20 | 41/20 | 41/30 | 52 | 44 | $\underline{20}$ | 32 | 21 | 31 | 28 |
|  | DR2C | 41/20 | 41/20 | 41/22 | 52 | 39 | $\underline{20}$ | 32 | 21 | 31 | 25 |
|  | DR2D | 41/20 | 41/20 | 41/25 | 52 | 37 | 20 | 30 | 22 | 32 | 26 |
|  | FARINON DMI/2 | 41/20 | 41/20 | 41/35 | 55 | 47 | 22 | 41 | 22 | 26 | 29 |
|  | VIDAR DRM2-6 | 41/20 | 41/20 | 41/23 | 52 | 38 | $\underline{20}$ | 30 | 21 | 32 | 24 |
|  | LENKURT 79FI-D | 41/20 | 41/20 | 41/30 | 50 | 38 | $\underline{20}$ | 33 | 22 | 32 | 32 |

Note 1: All underlined objectives are floor numbers.
Note 2: $X X / Y Y-X X$ is a threshold degradation number based on a 40 dB typical fade margin for nominal system IF filtering in the analog group. The objective may be relaxed dB for dB up to $\mathrm{Y} Y$ for lesser margins.
table G
2-GHz INTERFERENCE OBJECTIVES
4.8-MHz SEPARATION
interfered-with systems

|  | SYSTEM | 72 | 132 | 252 | NEC-STD | NEC-HI | DR2C | DR2D | farinon DM1/2 | VIDAR DRM2-6 | LENKURT <br> 79F1-D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 72 | 24/20 | 24/20 | 24/20 | 27 | $\underline{20}$ | $\underline{20}$ | $\underline{20}$ | 23 | 21 | $\underline{20}$ |
|  | 132 | 23/20 | 23/20 | 23/20 | 26 | $\underline{20}$ | $\underline{20}$ | $\underline{20}$ | 22 | 22 | $\underline{20}$ |
|  | 252 | 22/20 | 22/20 | 22/20 | 26 | $\underline{20}$ | 20 | 20 | 22 | 22 | $\underline{20}$ |
|  | NEC.STD | 32/20 | 32/20 | 32/20 | 31 | $\underline{20}$ | $\underline{20}$ | 20 | 23 | 20 | $\underline{20}$ |
|  | NEC.HI | 32/20 | 32/20 | 32/20 | 31 | $\underline{20}$ | $\underline{20}$ | $\underline{20}$ | 23 | 20 | 20 |
|  | DR2C | 32/20 | 32/20 | 32/20 | 30 | $\underline{20}$ | $\underline{20}$ | $\underline{20}$ | 23 | 20 | $\underline{20}$ |
|  | DR2D | 31/20 | 31/20 | 31/20 | 30 | $\underline{20}$ | $\underline{20}$ | $\underline{20}$ | 23 | $\underline{20}$ | $\underline{20}$ |
|  | FARINON DMI/2 | 40/20 | 40/20 | 40/20 | 36 | $\underline{20}$ | $\underline{20}$ | 20 | 23 | $\underline{20}$ | $\underline{20}$ |
|  | VIDAR DRM2-6 | 32/20 | 32/20 | 32/20 | 30 | $\underline{20}$ | $\underline{20}$ | 20 | 23 | $\underline{20}$ | $\underline{20}$ |
|  | LeNKURT T9FI-D | 40/20 | 40/20 | 40/20 | 32 | $\underline{20}$ | 20 | 20 | 23 | 20 | $\underline{2}$ |

Note 1: All underlined objectives are floor numbers.
Note 2: $\mathrm{XX} / \mathrm{YY}-\mathrm{XX}$ is a threshold degradation number based on a $40-\mathrm{dB}$ typical fade margin for nominal system IF filtering in the analog group. The objective may be relaxed dB for dB up to YY for lesser fade margins.

